

## GA - General Aptitude

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### Q1 - Q5 carry one mark each.

- Q.No. 1** This book, including all its chapters, \_\_\_\_\_ interesting. The students as well as the instructor \_\_\_\_\_ in agreement about it.
- (A) is, was  
(B) are, are  
(C) is, are  
(D) were, was
- Q.No. 2** People were prohibited \_\_\_\_\_ their vehicles near the entrance of the main administrative building.
- (A) to park  
(B) from parking  
(C) parking  
(D) to have parked
- Q.No. 3** Select the word that fits the analogy:
- Do : Undo :: Trust : \_\_\_\_\_
- (A) Entrust  
(B) Intrust  
(C) Distrust  
(D) Untrust
- Q.No. 4** Stock markets \_\_\_\_\_ at the news of the coup.
- (A) poised  
(B) plunged  
(C) plugged  
(D) probed
- Q.No. 5** If  $P, Q, R, S$  are four individuals, how many teams of size exceeding one can be formed, with  $Q$  as a member?
- (A) 5  
(B) 6  
(C) 7  
(D) 8

### Q6 - Q10 carry two mark each.

- Q.No. 6** Non-performing Assets (NPAs) of a bank in India is defined as an asset, which remains unpaid by a borrower for a certain period of time in terms of interest, principal, or both. Reserve Bank of India (RBI) has changed the definition of NPA thrice during 1993-2004, in terms of the holding period of loans. The holding period was reduced by one quarter each time. In 1993, the holding period was four quarters (360 days).
- Based on the above paragraph, the holding period of loans in 2004 after the third revision was \_\_\_\_\_ days.
- (A) 45  
(B) 90  
(C) 135  
(D) 180

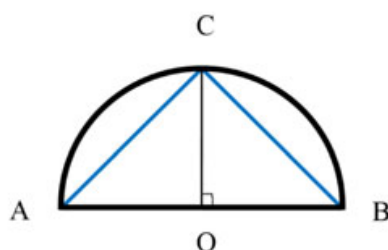
**Q.No. 7** Select the next element of the series: Z, WV, RQP, \_\_\_\_

- (A) LKJI
- (B) JIHG
- (C) KJIH
- (D) NMLK

**Q.No. 8** In four-digit integer numbers from 1001 to 9999, the digit group “37” (in the same sequence) appears \_\_\_\_\_ times.

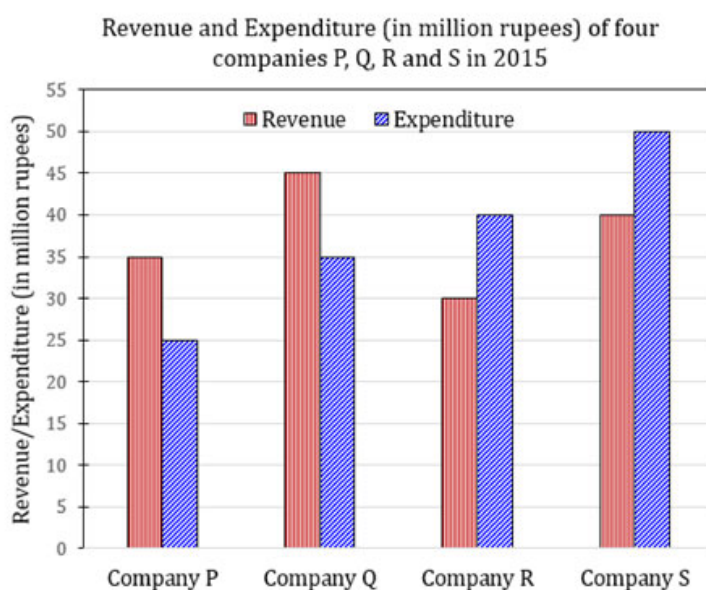
- (A) 270
- (B) 279
- (C) 280
- (D) 299

**Q.No. 9** Given a semicircle with  $O$  as the centre, as shown in the figure, the ratio  $\frac{\overline{AC} + \overline{CB}}{\overline{AB}}$  is \_\_\_\_\_, where  $\overline{AC}$ ,  $\overline{CB}$  and  $\overline{AB}$  are chords.



- (A)  $\sqrt{2}$
- (B)  $\sqrt{3}$
- (C) 2
- (D) 3

**Q.No. 10** The revenue and expenditure of four different companies P, Q, R and S in 2015 are shown in the figure. If the revenue of company Q in 2015 was 20% more than that in 2014, and company Q had earned a profit of 10% on expenditure in 2014, then its expenditure (in million rupees) in 2014 was \_\_\_\_\_.



- (A) 32.7
- (B) 33.7
- (C) 34.1
- (D) 35.1

- Q.No. 1**  $ax^3 + bx^2 + cx + d$  is a polynomial on real  $x$  over real coefficients  $a, b, c, d$  wherein  $a \neq 0$ . Which of the following statements is true?
- (A)  $d$  can be chosen to ensure that  $x = 0$  is a root for any given set  $a, b, c$ .  
 (B) No choice of coefficients can make all roots identical.  
 (C)  $a, b, c, d$  can be chosen to ensure that all roots are complex.  
 (D)  $c$  alone cannot ensure that all roots are real.
- Q.No. 2** Which of the following is true for all possible non-zero choices of integers  $m, n; m \neq n$ , or all possible non-zero choices of real numbers  $p, q; p \neq q$ , as applicable?
- (A)  $\frac{1}{\pi} \int_0^\pi \sin m\theta \sin n\theta d\theta = 0$   
 (B)  $\frac{1}{2\pi} \int_{-\pi/2}^{\pi/2} \sin p\theta \sin q\theta d\theta = 0$   
 (C)  $\frac{1}{2\pi} \int_{-\pi}^\pi \sin p\theta \cos q\theta d\theta = 0$   
 (D)  $\lim_{\alpha \rightarrow \infty} \frac{1}{2\alpha} \int_{-\alpha}^\alpha \sin p\theta \sin q\theta d\theta = 0$
- Q.No. 3** Which of the following statements is true about the two sided Laplace transform?
- (A) It exists for every signal that may or may not have a Fourier transform.  
 (B) It has no poles for any bounded signal that is non-zero only inside a finite time interval.  
 (C) The number of finite poles and finite zeroes must be equal.  
 (D) If a signal can be expressed as a weighted sum of shifted one sided exponentials, then its Laplace Transform will have no poles.
- Q.No. 4** Consider a signal  $x[n] = \left(\frac{1}{2}\right)^n 1[n]$ , where  $1[n] = 0$  if  $n < 0$ , and  $1[n] = 1$  if  $n \geq 0$ . The z-transform of  $x[n - k]$ ,  $k > 0$  is  $\frac{z^{-k}}{1 - \frac{1}{2} z^{-1}}$  with region of convergence being
- (A)  $|z| < 2$   
 (B)  $|z| > 2$   
 (C)  $|z| < 1/2$   
 (D)  $|z| > 1/2$
- Q.No. 5** The value of the following complex integral, with  $C$  representing the unit circle centered at origin in the counterclockwise sense, is:

$$\int_C \frac{z^2 + 1}{z^2 - 2z} dz$$

- (A)  $8\pi i$   
 (B)  $-8\pi i$   
 (C)  $-\pi i$   
 (D)  $\pi i$

- Q.No. 6**  $x_R$  and  $x_A$  are, respectively, the rms and average values of  $x(t) = x(t - T)$ , and similarly,  $y_R$  and  $y_A$  are, respectively, the rms and average values of  $y(t) = kx(t)$ .  $k, T$  are independent of  $t$ . Which of the following is true?
- (A)  $y_A = kx_A; y_R = kx_R$
  - (B)  $y_A = kx_A; y_R \neq kx_R$
  - (C)  $y_A \neq kx_A; y_R = kx_R$
  - (D)  $y_A \neq kx_A; y_R \neq kx_R$

- Q.No. 7** A three-phase cylindrical rotor synchronous generator has a synchronous reactance  $X_s$  and a negligible armature resistance. The magnitude of per phase terminal voltage is  $V_A$  and the magnitude of per phase induced emf is  $E_A$ . Considering the following two statements, P and Q,

P: For any three-phase balanced leading load connected across the terminals of this synchronous generator,  $V_A$  is always more than  $E_A$

Q: For any three-phase balanced lagging load connected across the terminals of this synchronous generator,  $V_A$  is always less than  $E_A$

which of the following options is correct?

- (A) P is false and Q is true.
- (B) P is true and Q is false.
- (C) P is false and Q is false.
- (D) P is true and Q is true.

- Q.No. 8** A lossless transmission line with 0.2 pu reactance per phase uniformly distributed along the length of the line, connecting a generator bus to a load bus, is protected up to 80 % of its length by a distance relay placed at the generator bus. The generator terminal voltage is 1 pu. There is no generation at the load bus. The threshold pu current for operation of the distance relay for a solid three phase-to-ground fault on the transmission line is closest to:

- (A) 1.00
- (B) 3.61
- (C) 5.00
- (D) 6.25

- Q.No. 9** Out of the following options, the most relevant information needed to specify the real power (P) at the PV buses in a load flow analysis is

- (A) solution of economic load dispatch
- (B) rated power output of the generator
- (C) rated voltage of the generator
- (D) base power of the generator

**Q.No. 10**

Consider a linear time-invariant system whose input  $r(t)$  and output  $y(t)$  are related by the following differential equation:

$$\frac{d^2 y(t)}{dt^2} + 4y(t) = 6r(t)$$

The poles of this system are at

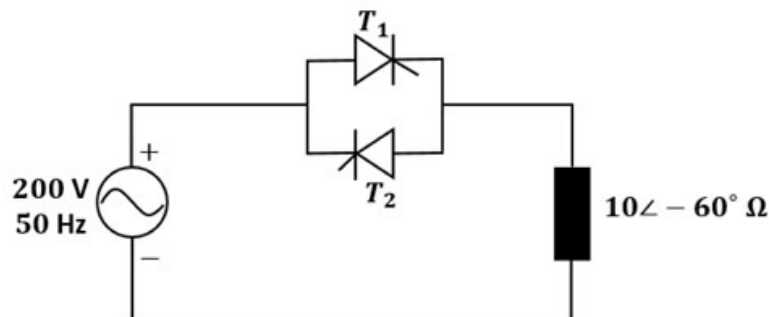
- (A)  $+2j, -2j$
- (B)  $+2, -2$
- (C)  $+4, -4$
- (D)  $+4j, -4j$

**Q.No. 11** A single-phase, full-bridge diode rectifier fed from a 230 V, 50 Hz sinusoidal source supplies a series combination of finite resistance,  $R$ , and a very large inductance,  $L$ . The two most dominant frequency components in the source

current are:

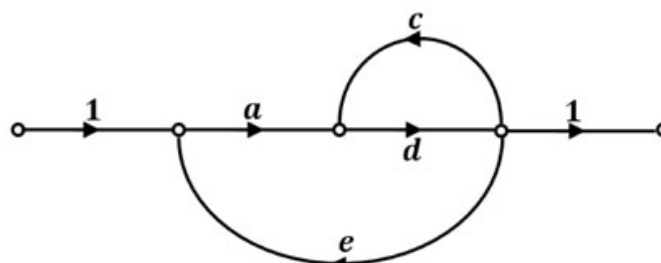
- (A) 50 Hz, 0 Hz
- (B) 50 Hz, 100 Hz
- (C) 50 Hz, 150 Hz
- (D) 150 Hz, 250 Hz

**Q.No. 12** Thyristor  $T_1$  is triggered at an angle  $\alpha$  (in degree), and  $T_2$  at angle  $180^\circ + \alpha$ , in each cycle of the sinusoidal input voltage. Assume both thyristors to be ideal. To control the load power over the range 0 to 2 kW, the minimum range of variation in  $\alpha$  is:

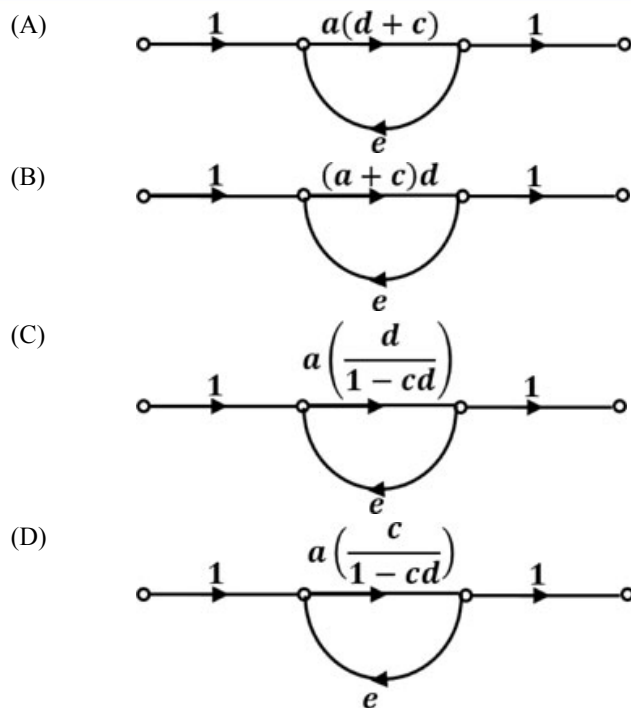


- (A)  $0^\circ$  to  $60^\circ$
- (B)  $0^\circ$  to  $120^\circ$
- (C)  $60^\circ$  to  $120^\circ$
- (D)  $60^\circ$  to  $180^\circ$

**Q.No. 13** Which of the options is an equivalent representation of the signal flow graph shown here?







**Q.No. 14** A common-source amplifier with a drain resistance,  $R_D = 4.7 \text{ k}\Omega$ , is powered using a 10 V power supply. Assuming that the transconductance,  $g_m$ , is  $520 \mu\text{A/V}$ , the voltage gain of the amplifier is closest to:

- (A) -2.44  
(B) -1.22  
(C) 1.22  
(D) 2.44

**Q.No. 15** A sequence detector is designed to detect precisely 3 digital inputs, with overlapping sequences detectable. For the sequence (1,0,1) and input data (1,1,0,1,0,0,1,1,0,1,0,1,1,0), what is the output of this detector?

- (A) 1,1,0,0,0,0,1,1,0,1,0,0  
(B) 0,1,0,0,0,0,0,1,0,1,0,0  
(C) 0,1,0,0,0,0,0,1,0,1,1,0  
(D) 0,1,0,0,0,0,0,0,1,0,0,0

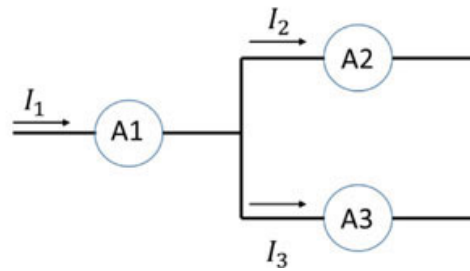
**Q.No. 16** Consider the initial value problem below. The value of  $y$  at  $x = \ln 2$ , (rounded off to 3 decimal places) is \_\_\_\_\_.

$$\frac{dy}{dx} = 2x - y, \quad y(0) = 1$$

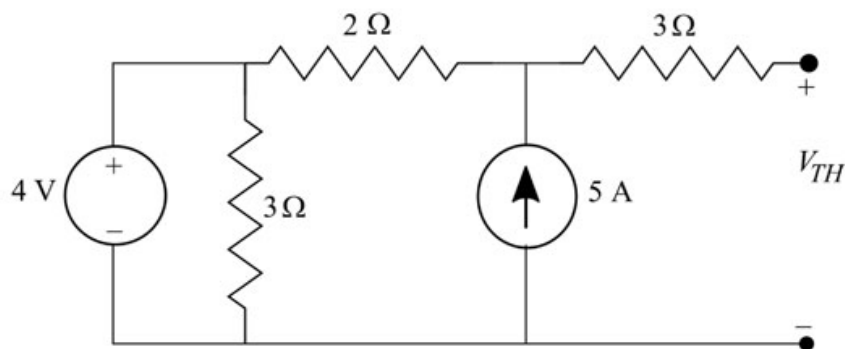
**Q.No. 17** A three-phase, 50 Hz, 4-pole induction motor runs at no-load with a slip of 1 %. With full load, the slip increases to 5 %. The % speed regulation of the motor (rounded off to 2 decimal places) is \_\_\_\_\_.

**Q.No. 18**

Currents through ammeters A2 and A3 in the figure are  $1\angle 10^\circ$  and  $1\angle 70^\circ$ , respectively. The reading of the ammeter A1 (rounded off to 3 decimal places) is \_\_\_\_\_ A.

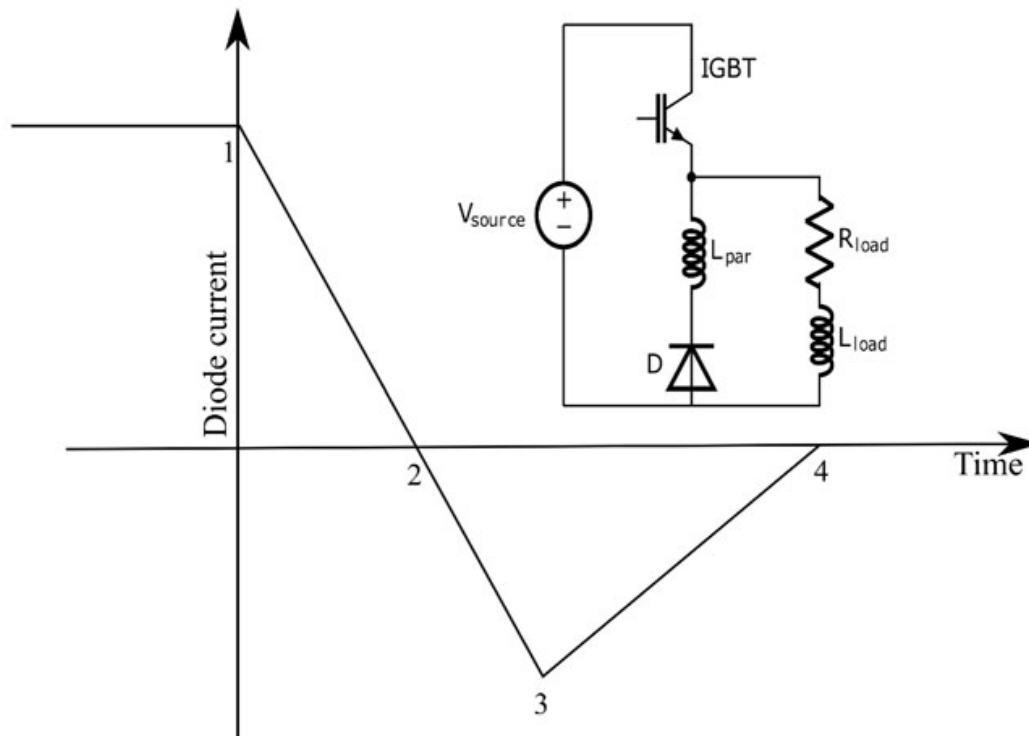


Q.No. 19 The Thevenin equivalent voltage,  $V_{TH}$ , in V (rounded off to 2 decimal places) of the network shown below, is \_\_\_\_\_



Q.No. 20

A double pulse measurement for an inductively loaded circuit controlled by the IGBT switch is carried out to evaluate the reverse recovery characteristics of the diode, D, represented approximately as a piecewise linear plot of current vs time at diode turn-off.  $L_{par}$  is a parasitic inductance due to the wiring of the circuit, and is in series with the diode. The point on the plot (indicate your choice by entering 1, 2, 3 or 4) at which the IGBT experiences the highest current stress is \_\_\_\_\_.

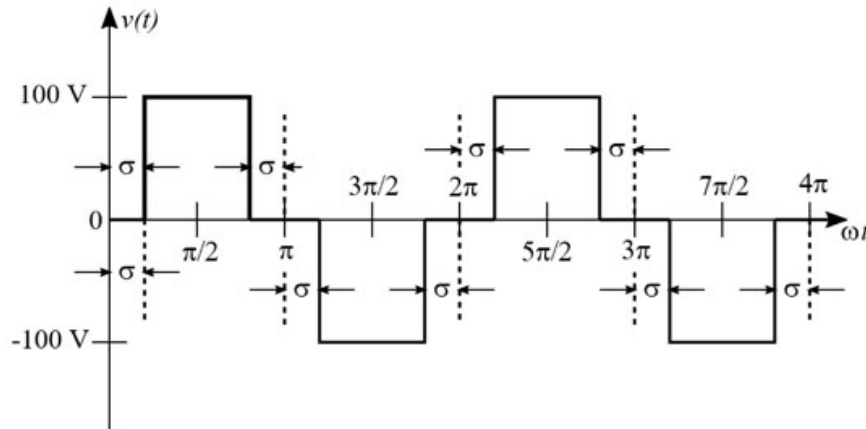


**Q.No. 21** A single-phase, 4 kVA, 200 V/100 V, 50 Hz transformer with laminated CRGO steel core has rated no-load loss of 450 W. When the high-voltage winding is excited with 160 V, 40 Hz sinusoidal ac supply, the no-load losses are found to be 320 W. When the high-voltage winding of the same transformer is supplied from a 100 V, 25 Hz sinusoidal ac source, the no-load losses will be \_\_\_\_\_ W (rounded off to 2 decimal places).

**Q.No. 22**



A single-phase inverter is fed from a 100 V dc source and is controlled using a quasi-square wave modulation scheme to produce an output waveform,  $v(t)$ , as shown. The angle  $\sigma$  is adjusted to entirely eliminate the 3<sup>rd</sup> harmonic component from the output voltage. Under this condition, for  $v(t)$ , the magnitude of the 5<sup>th</sup> harmonic component as a percentage of the magnitude of the fundamental component is \_\_\_\_\_ (rounded off to 2 decimal places).

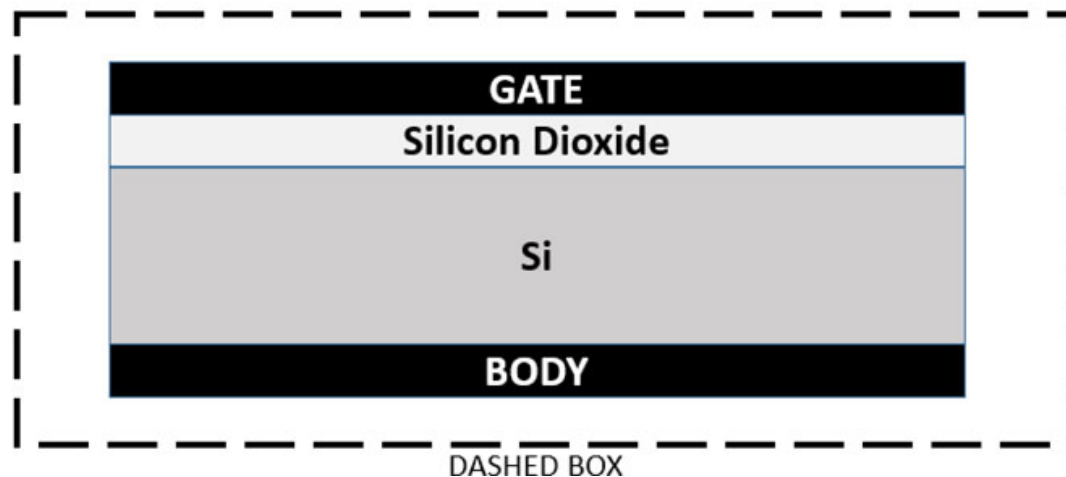


Q.No. 23 A single 50 Hz synchronous generator on droop control was delivering 100 MW power to a system. Due to increase in load, generator power had to be increased by 10 MW, as a result of which, system frequency dropped to 49.75 Hz. Further increase in load in the system resulted in a frequency of 49.25 Hz. At this condition, the power in MW supplied by the generator is \_\_\_\_\_ (rounded off to 2 decimal places).

Q.No. 24 Consider a negative unity feedback system with forward path transfer function  $G(s) = \frac{K}{(s+a)(s-b)(s+c)}$ , where  $K, a, b, c$  are positive real numbers. For a Nyquist path enclosing the entire imaginary axis and right half of the  $s$ -plane in the clockwise direction, the Nyquist plot of  $(1 + G(s))$ , encircles the origin of  $(1 + G(s))$ -plane once in the clockwise direction and never passes through this origin for a certain value of  $K$ . Then, the number of poles of  $\frac{G(s)}{1+G(s)}$  lying in the open right half of the  $s$ -plane is \_\_\_\_\_.

Q.No. 25

The cross-section of a metal-oxide-semiconductor structure is shown schematically. Starting from an uncharged condition, a bias of +3 V is applied to the gate contact with respect to the body contact. The charge inside the silicon dioxide layer is then measured to be  $+Q$ . The total charge contained within the dashed box shown, upon application of bias, expressed as a multiple of  $Q$  (absolute value in Coulombs, rounded off to the nearest integer) is \_\_\_\_\_.



- Q.No. 26** For real numbers,  $x$  and  $y$ , with  $y = 3x^2 + 3x + 1$ , the maximum and minimum value of  $y$  for  $x \in [-2, 0]$  are respectively, \_\_\_\_\_.
- (A) 7 and  $1/4$ .  
 (B) 7 and 1.  
 (C)  $-2$  and  $-1/2$ .  
 (D) 1 and  $1/4$ .

- Q.No. 27** The vector function expressed by

$$\mathbf{F} = \mathbf{a}_x (5y - k_1 z) + \mathbf{a}_y (3z + k_2 x) + \mathbf{a}_z (k_3 y - 4x)$$

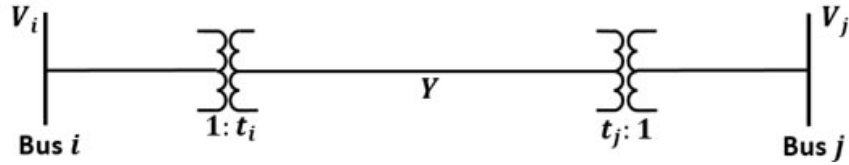
represents a conservative field, where  $\mathbf{a}_x, \mathbf{a}_y, \mathbf{a}_z$  are unit vectors along  $x, y$  and  $z$  directions, respectively. The values of constants  $k_1, k_2, k_3$  are given by:

- (A)  $k_1 = 3, k_2 = 3, k_3 = 7$   
 (B)  $k_1 = 3, k_2 = 8, k_3 = 5$   
 (C)  $k_1 = 4, k_2 = 5, k_3 = 3$   
 (D)  $k_1 = 0, k_2 = 0, k_3 = 0$

- Q.No. 28** A 250 V dc shunt motor has an armature resistance of  $0.2 \Omega$  and a field resistance of  $100 \Omega$ . When the motor is operated on no-load at rated voltage, it draws an armature current of 5 A and runs at 1200 rpm. When a load is coupled to the motor, it draws total line current of 50 A at rated voltage, with a 5 % reduction in the air-gap flux due to armature reaction. Voltage drop across the brushes can be taken as 1 V per brush under all operating conditions. The speed of the motor, in rpm, under this loaded condition, is closest to:
- (A) 1200  
 (B) 1000

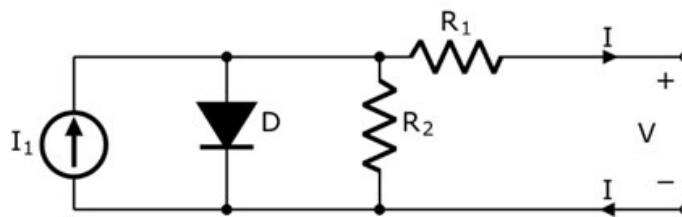
- (C) 1220  
(D) 900

**Q.No. 29** Two buses,  $i$  and  $j$ , are connected with a transmission line of admittance  $Y$ , at the two ends of which there are ideal transformers with turns ratios as shown. Bus admittance matrix for the system is:



- (A)  $\begin{bmatrix} -t_i t_j Y & t_j^2 Y \\ t_i^2 Y & -t_i t_j Y \end{bmatrix}$   
 (B)  $\begin{bmatrix} t_i t_j Y & -t_j^2 Y \\ -t_i^2 Y & t_i t_j Y \end{bmatrix}$   
 (C)  $\begin{bmatrix} t_i^2 Y & -t_i t_j Y \\ -t_i t_j Y & t_j^2 Y \end{bmatrix}$   
 (D)  $\begin{bmatrix} t_i t_j Y & -(t_i - t_j)^2 Y \\ -(t_i - t_j)^2 Y & t_i t_j Y \end{bmatrix}$

**Q.No. 30** Consider the diode circuit shown below. The diode,  $D$ , obeys the current-voltage characteristic  $I_D = I_S \left( \exp \left( \frac{V_D}{nV_T} \right) - 1 \right)$ , where  $n > 1$ ,  $V_T > 0$ ,  $V_D$  is the voltage across the diode and  $I_D$  is the current through it. The circuit is biased so that voltage,  $V > 0$  and current,  $I < 0$ . If you had to design this circuit to transfer maximum power from the current source ( $I_1$ ) to a resistive load (not shown) at the output, what values of  $R_1$  and  $R_2$  would you choose?



- (A) Large  $R_1$  and large  $R_2$ .  
 (B) Small  $R_1$  and small  $R_2$ .  
 (C) Large  $R_1$  and small  $R_2$ .  
 (D) Small  $R_1$  and large  $R_2$ .

**Q.No. 31** A non-ideal diode is biased with a voltage of  $-0.03$  V, and a diode current of  $I_1$  is measured. The thermal voltage is 26 mV and the ideality factor for the diode is 15/13. The voltage, in V, at which the measured current increases to  $1.5I_1$  is closest to:

- (A)  $-0.02$   
 (B)  $-0.09$   
 (C)  $-1.50$   
 (D)  $-4.50$

**Q.No. 32** A benchtop dc power supply acts as an ideal 4 A current source as long as its terminal voltage is below 10 V. Beyond this point, it begins to behave as an ideal 10 V voltage source for all load currents going down to 0 A. When connected to an ideal rheostat, find the load resistance value at which maximum power is transferred, and the corresponding load voltage and current.

- (A) Short,  $\infty$  A, 10 V
- (B) Open, 4 A, 0 V
- (C)  $2.5 \Omega$ , 4 A, 10 V
- (D)  $2.5 \Omega$ , 4 A, 5 V

**Q.No. 33** The static electric field inside a dielectric medium with relative permittivity,  $\epsilon_r = 2.25$ , expressed in cylindrical coordinate system is given by the following expression

$$\mathbf{E} = \mathbf{a}_r 2r + \mathbf{a}_\phi \left( \frac{3}{r} \right) + \mathbf{a}_z 6$$

where  $\mathbf{a}_r$ ,  $\mathbf{a}_\phi$ ,  $\mathbf{a}_z$  are unit vectors along  $r$ ,  $\phi$  and  $z$  directions, respectively. If the above expression represents a valid electrostatic field inside the medium, then the volume charge density associated with this field in terms of free space permittivity,  $\epsilon_0$ , in SI units is given by:

- (A)  $3\epsilon_0$
- (B)  $4\epsilon_0$
- (C)  $5\epsilon_0$
- (D)  $9\epsilon_0$

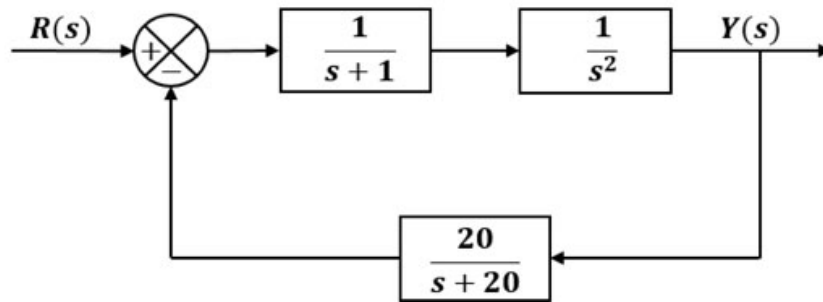
**Q.No. 34** Consider a permanent magnet dc (PMDC) motor which is initially at rest. At  $t = 0$ , a dc voltage of 5 V is applied to the motor. Its speed monotonically increases from 0 rad/s to 6.32 rad/s in 0.5 s and finally settles to 10 rad/s. Assuming that the armature inductance of the motor is negligible, the transfer function for the motor is

- (A)  $\frac{10}{0.5s+1}$
- (B)  $\frac{2}{0.5s+1}$
- (C)  $\frac{10}{s+0.5}$
- (D)  $\frac{2}{s+0.5}$

**Q.No. 35**



Which of the following options is correct for the system shown below?



- (A) 4<sup>th</sup> order and stable
- (B) 3<sup>rd</sup> order and stable
- (C) 4<sup>th</sup> order and unstable
- (D) 3<sup>rd</sup> order and unstable

**Q.No. 36** Consider a negative unity feedback system with the forward path transfer function

$$\frac{s^2 + s + 1}{s^3 + 2s^2 + 2s + K}, \text{ where } K \text{ is a positive real number. The value of } K \text{ for which the}$$

system will have some of its poles on the imaginary axis is \_\_\_\_\_.

- (A) 9
- (B) 8
- (C) 7
- (D) 6

**Q.No. 37** Suppose for input  $x(t)$  a linear time-invariant system with impulse response  $h(t)$  produces output  $y(t)$ , so that  $x(t) * h(t) = y(t)$ . Further, if  $|x(t)| * |h(t)| = z(t)$ , which of the following statements is true?

- (A) For all  $t \in (-\infty, \infty)$ ,  $z(t) \leq y(t)$
- (B) For some but not all  $t \in (-\infty, \infty)$ ,  $z(t) \leq y(t)$
- (C) For all  $t \in (-\infty, \infty)$ ,  $z(t) \geq y(t)$
- (D) For some but not all  $t \in (-\infty, \infty)$ ,  $z(t) \geq y(t)$

**Q.No. 38** The causal realization of a system transfer function  $H(s)$  having poles at  $(2, -1), (-2, 1)$  and zeroes at  $(2, 1), (-2, -1)$  will be

- (A) stable, real, allpass
- (B) unstable, complex, allpass
- (C) unstable, real, highpass
- (D) stable, complex, lowpass

**Q.No. 39** Which of the following options is true for a linear time-invariant discrete time system that obeys the difference equation:

$$y[n] - ay[n - 1] = b_0x[n] - b_1x[n - 1]$$

- (A)  $y[n]$  is unaffected by the values of  $x[n - k]; k > 2$ .
- (B) The system is necessarily causal.
- (C) The system impulse response is non-zero at infinitely many instants.
- (D) When  $x[n] = 0, n < 0$ , the function  $y[n]; n > 0$  is solely determined by the function  $x[n]$ .



**Q.No. 40** Let  $\mathbf{a}_r$ ,  $\mathbf{a}_\phi$  and  $\mathbf{a}_z$  be unit vectors along  $r$ ,  $\phi$  and  $z$  directions, respectively in the cylindrical coordinate system. For the electric flux density given by  $\mathbf{D} = (\mathbf{a}_r 15 + \mathbf{a}_\phi 2r - \mathbf{a}_z 3rz)$  Coulomb/m<sup>2</sup>, the total electric flux, in Coulomb, emanating from the volume enclosed by a solid cylinder of radius 3 m and height 5 m oriented along the  $z$ -axis with its base at the origin is:

- (A)  $54 \pi$
- (B)  $90 \pi$
- (C)  $108 \pi$
- (D)  $180 \pi$

**Q.No. 41** A stable real linear time-invariant system with single pole at  $p$ , has a transfer function  $H(s) = \frac{s^2+100}{s-p}$  with a dc gain of 5. The smallest positive frequency, in rad/s, at unity gain is closest to:

- (A) 8.84
- (B) 11.08
- (C) 78.13
- (D) 122.87

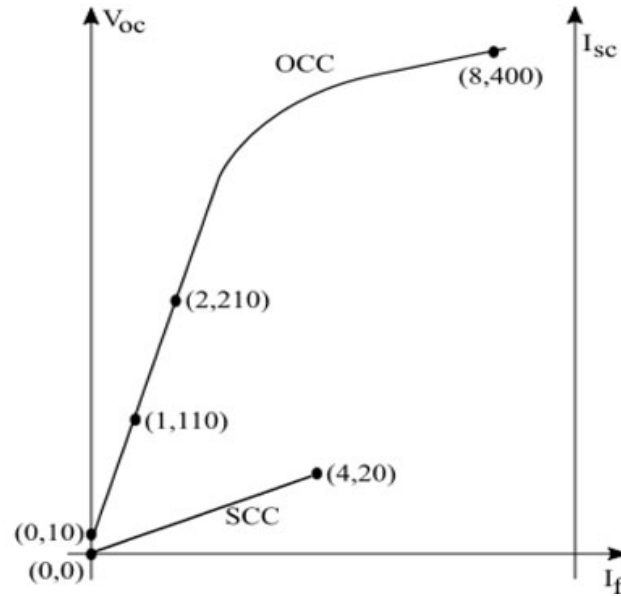
**Q.No. 42** The number of purely real elements in a lower triangular representation of the given  $3 \times 3$  matrix, obtained through the given decomposition is \_\_\_\_\_.

$$\begin{bmatrix} 2 & 3 & 3 \\ 3 & 2 & 1 \\ 3 & 1 & 7 \end{bmatrix} = \begin{bmatrix} a_{11} & 0 & 0 \\ a_{12} & a_{22} & 0 \\ a_{13} & a_{23} & a_{33} \end{bmatrix} \begin{bmatrix} a_{11} & 0 & 0 \\ a_{12} & a_{22} & 0 \\ a_{13} & a_{23} & a_{33} \end{bmatrix}^T$$

- (A) 5
- (B) 6
- (C) 8
- (D) 9

**Q.No. 43**

The figure below shows the per-phase Open Circuit Characteristics (measured in V) and Short Circuit Characteristics (measured in A) of a 14 kVA, 400 V, 50 Hz, 4-pole, 3-phase, delta connected alternator, driven at 1500 rpm. The field current,  $I_f$  is measured in A. Readings taken are marked as respective (x, y) coordinates in the figure. Ratio of the unsaturated and saturated synchronous impedances ( $Z_{s(unsat)}/Z_{s(sat)}$ ) of the alternator is closest to:



- (A) 2.100
- (B) 2.025
- (C) 2.000
- (D) 1.000

Q.No. 44

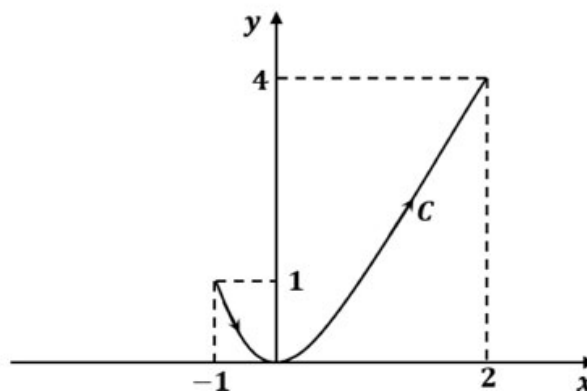
Let  $\mathbf{a}_x$  and  $\mathbf{a}_y$  be unit vectors along x and y directions, respectively. A vector function is given by

$$\mathbf{F} = \mathbf{a}_x y - \mathbf{a}_y x$$

The line integral of the above function

$$\int_C \mathbf{F} \cdot d\mathbf{l}$$

along the curve  $C$ , which follows the parabola  $y = x^2$  as shown below is \_\_\_\_\_ (rounded off to 2 decimal places).



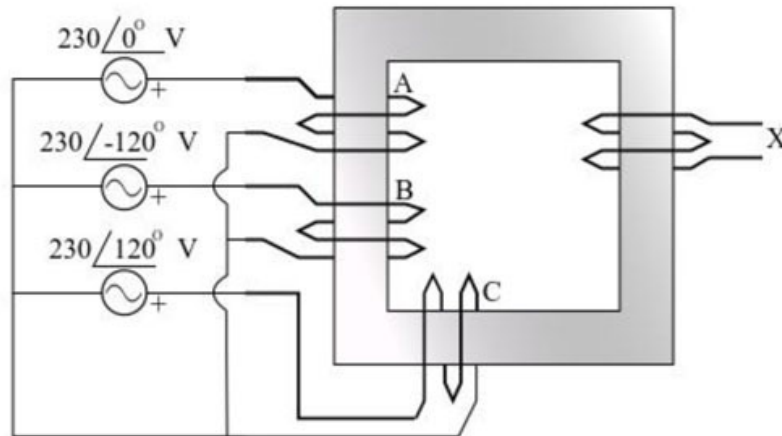
- Q.No. 45 A resistor and a capacitor are connected in series to a 10 V dc supply through a switch. The switch is closed at  $t = 0$ , and the capacitor voltage is found to cross 0 V at  $t = 0.4\tau$ , where  $\tau$  is the circuit time constant. The absolute value of percentage change required in the initial capacitor voltage if the zero crossing has to happen at  $t = 0.2\tau$  is \_\_\_\_\_ (rounded off to 2 decimal places).
- Q.No. 46 A cylindrical rotor synchronous generator with constant real power output and constant terminal voltage is supplying 100 A current to a 0.9 lagging power factor load. An ideal reactor is now connected in parallel with the load, as a result of which the total lagging reactive power requirement of the load is twice the previous value while the real power remains unchanged. The armature current is now \_\_\_\_\_ A (rounded off to 2 decimal places).

Q.No. 47

Bus 1 with voltage magnitude  $V_1 = 1.1$  pu is sending reactive power  $Q_{12}$  towards bus 2 with voltage magnitude  $V_2 = 1$  pu through a lossless transmission line of reactance  $X$ . Keeping the voltage at bus 2 fixed at 1 pu, magnitude of voltage at bus 1 is changed, so that the reactive power  $Q_{12}$  sent from bus 1 is increased by 20%. Real power flow through the line under both the conditions is zero. The new value of the voltage magnitude,  $V_1$ , in pu (rounded off to 2 decimal places), at bus 1 is \_\_\_\_\_.



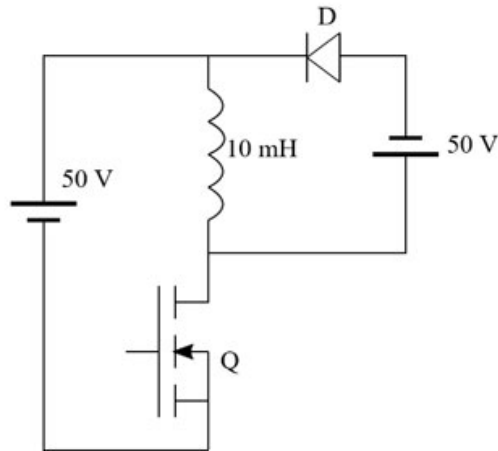
- Q.No. 48 Windings 'A', 'B' and 'C' have 20 turns each and are wound on the same iron core as shown, along with winding 'X' which has 2 turns. The figure shows the sense (clockwise/anti-clockwise) of each of the windings only and does not reflect the exact number of turns. If windings 'A', 'B' and 'C' are supplied with balanced 3-phase voltages at 50 Hz and there is no core saturation, the no-load RMS voltage (in V, rounded off to 2 decimal places) across winding 'X' is \_\_\_\_\_.



- Q.No. 49 A cylindrical rotor synchronous generator has steady state synchronous reactance of 0.7 pu and subtransient reactance of 0.2 pu. It is operating at  $(1 + j0)$  pu terminal voltage with an internal emf of  $(1 + j0.7)$  pu. Following a three-phase solid short circuit fault at the terminal of the generator, the magnitude of the subtransient internal emf (rounded off to 2 decimal places) is \_\_\_\_\_ pu.

Q.No. 50

In the dc-dc converter circuit shown, switch Q is switched at a frequency of 10 kHz with a duty ratio of 0.6. All components of the circuit are ideal, and the initial current in the inductor is zero. Energy stored in the inductor in mJ (rounded off to 2 decimal places) at the end of 10 complete switching cycles is \_\_\_\_\_.

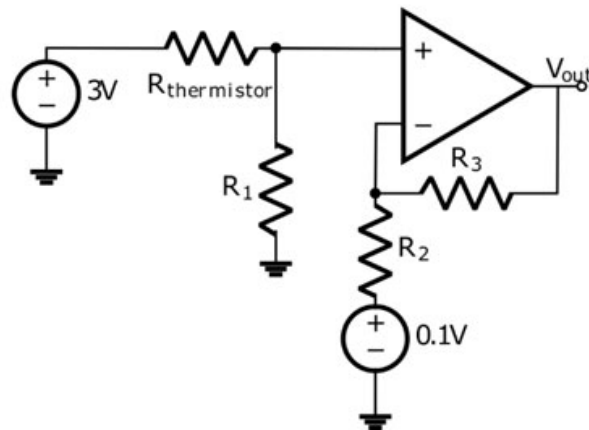


- Q.No. 51** A single-phase, full-bridge, fully controlled thyristor rectifier feeds a load comprising a  $10\ \Omega$  resistance in series with a very large inductance. The rectifier is fed from an ideal 230 V, 50 Hz sinusoidal source through cables which have negligible internal resistance and a total inductance of 2.28 mH. If the thyristors are triggered at an angle  $\alpha = 45^\circ$ , the commutation overlap angle in degree (rounded off to 2 decimal places) is \_\_\_\_\_.
- Q.No. 52** A non-ideal Si-based pn junction diode is tested by sweeping the bias applied across its terminals from  $-5\text{ V}$  to  $+5\text{ V}$ . The effective thermal voltage,  $V_T$ , for the diode is measured to be  $(29 \pm 2)\text{ mV}$ . The resolution of the voltage source in the measurement range is 1 mV. The percentage uncertainty (rounded off to 2 decimal places) in the measured current at a bias voltage of 0.02 V is \_\_\_\_\_.

**Q.No. 53**



The temperature of the coolant oil bath for a transformer is monitored using the circuit shown. It contains a thermistor with a temperature-dependent resistance,  $R_{thermistor} = 2 (1 + \alpha T)$  k $\Omega$ , where  $T$  is the temperature in  $^{\circ}\text{C}$ . The temperature coefficient,  $\alpha$ , is  $-(4 \pm 0.25) \text{ }^{\circ}\text{C}^{-1}$ . Circuit parameters:  $R_1 = 1 \text{ k}\Omega$ ,  $R_2 = 1.3 \text{ k}\Omega$ ,  $R_3 = 2.6 \text{ k}\Omega$ . The error in the output signal (in V, rounded off to 2 decimal places) at  $150^{\circ}\text{C}$  is \_\_\_\_\_.



Q.No. 54 An 8085 microprocessor accesses two memory locations (2001H) and (2002H), that contain 8-bit numbers 98H and B1H, respectively. The following program is executed:

LXI H,2001H

MVI A, 21H

INX H

ADD M

INX H

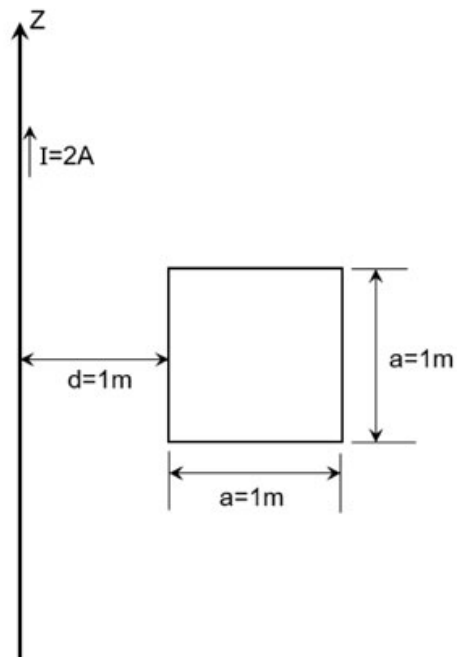
MOV M, A

HLT

At the end of this program, the memory location 2003H contains the number in decimal (base 10) form \_\_\_\_\_.

Q.No. 55

A conducting square loop of side length 1 m is placed at a distance of 1 m from a long straight wire carrying a current  $I = 2$  A as shown below. The mutual inductance, in nH (rounded off to 2 decimal places), between the conducting loop and the long wire is \_\_\_\_\_.



Q.No.	Session	Que.Type	Sec. Name	Key	Marks
1	5	MCQ	GA	C	1
2	5	MCQ	GA	B	1
3	5	MCQ	GA	C	1
4	5	MCQ	GA	B	1
5	5	MCQ	GA	C	1
6	5	MCQ	GA	B	2
7	5	MCQ	GA	C	2
8	5	MCQ	GA	B	2
9	5	MCQ	GA	A	2
10	5	MCQ	GA	C	2
1	5	MCQ	EE	A	1
2	5	MCQ	EE	D	1
3	5	MCQ	EE	B	1
4	5	MCQ	EE	D	1
5	5	MCQ	EE	C	1
6	5	MCQ	EE	A	1
7	5	MCQ	EE	A	1
8	5	MCQ	EE	D	1
9	5	MCQ	EE	A	1
10	5	MCQ	EE	A	1
11	5	MCQ	EE	C	1
12	5	MCQ	EE	D	1
13	5	MCQ	EE	C	1
14	5	MCQ	EE	A	1
15	5	MCQ	EE	B	1
16	5	NAT	EE	0.88000 to 0.88630	1
17	5	NAT	EE	4.10 to 4.40	1
18	5	NAT	EE	1.700 to 1.750	1
19	5	NAT	EE	13.80 to 14.20	1
20	5	NAT	EE	3 to 3	1
21	5	NAT	EE	162.41 to 162.59	1
22	5	NAT	EE	19.90 to 20.20	1
23	5	NAT	EE	125.00 to 135.00	1
24	5	NAT	EE	2 to 2	1
25	5	NAT	EE	0 to 0	1
26	5	MCQ	EE	A	2
27	5	MCQ	EE	C	2
28	5	MCQ	EE	C	2
29	5	MCQ	EE	C	2
30	5	MCQ	EE	D	2
31	5	MCQ	EE	B	2
32	5	MCQ	EE	C	2
33	5	MCQ	EE	D	2
34	5	MCQ	EE	B	2
35	5	MCQ	EE	C	2
36	5	MCQ	EE	B	2
37	5	MCQ	EE	C	2
38	5	MCQ	EE	B	2
39	5	MCQ	EE	C	2
40	5	MCQ	EE	D	2
41	5	MCQ	EE	A	2
42	5	MCQ	EE	C	2
43	5	MCQ	EE	B	2
44	5	NAT	EE	-3.05 to -2.95	2
45	5	NAT	EE	54.00 to 56.00	2
46	5	NAT	EE	123.00 to 127.00	2
47	5	NAT	EE	1.11 to 1.13	2
48	5	NAT	EE	45.90 to 46.10	2
49	5	NAT	EE	1.01 to 1.03	2
50	5	NAT	EE	4.95 to 5.05	2
51	5	NAT	EE	4.51 to 5.10	2
52	5	NAT	EE	11.50 to 12.00	2
53	5	NAT	EE	0.01 to 0.05	2
54	5	NAT	EE	210 to 210	2
55	5	NAT	EE	138.10 to 139.20	2